



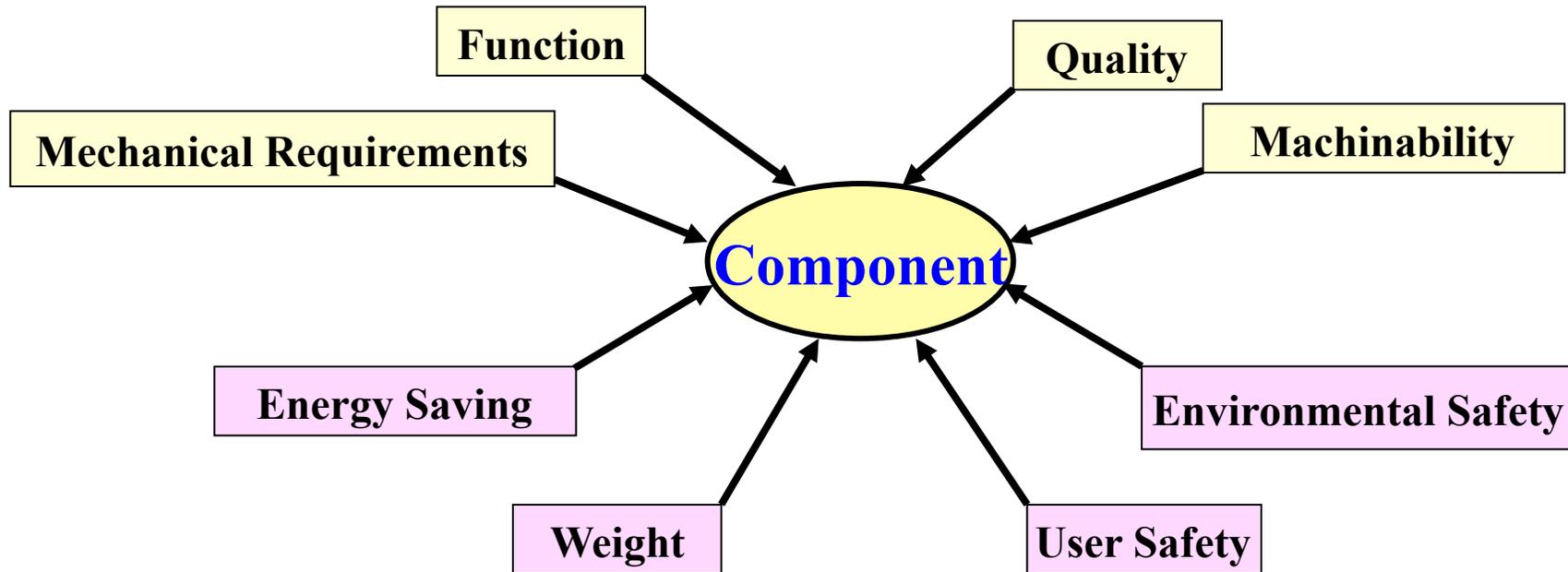
# **Nano-particle enhanced Transient Liquid Phase bonding process**

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United Kingdom**



# Why dissimilar joints?





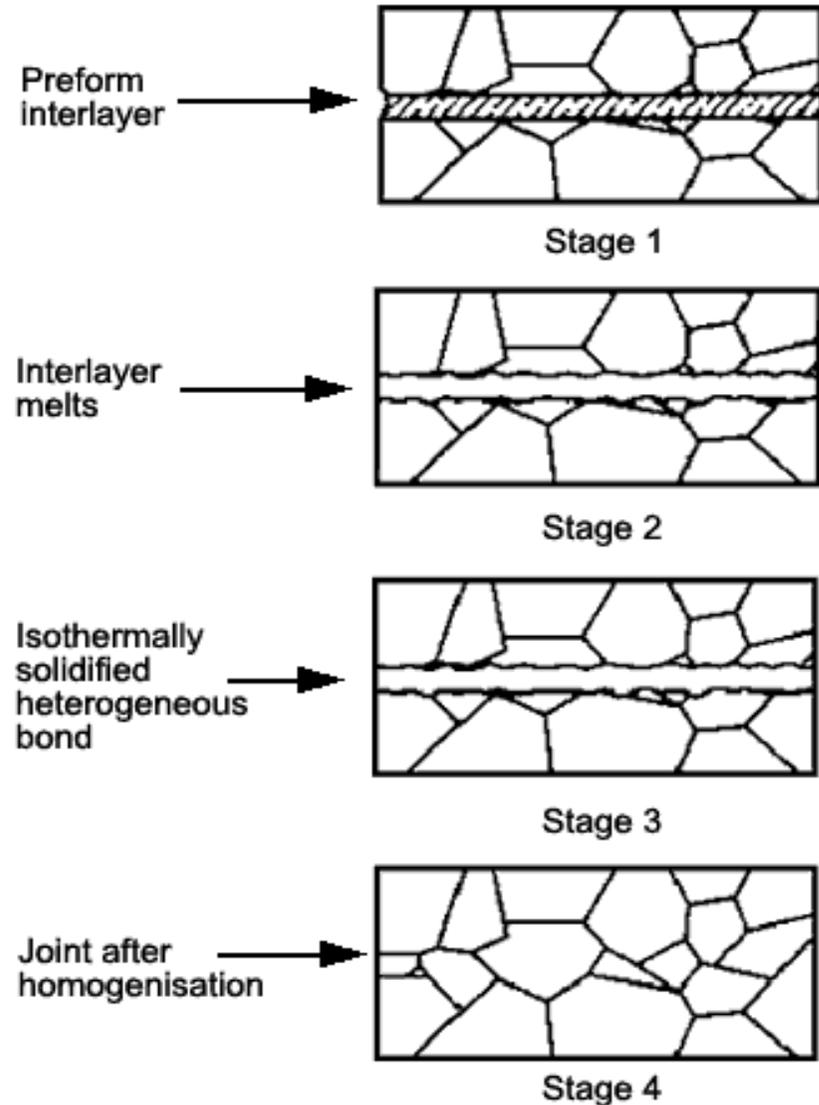
# Diffusion bonding apparatus



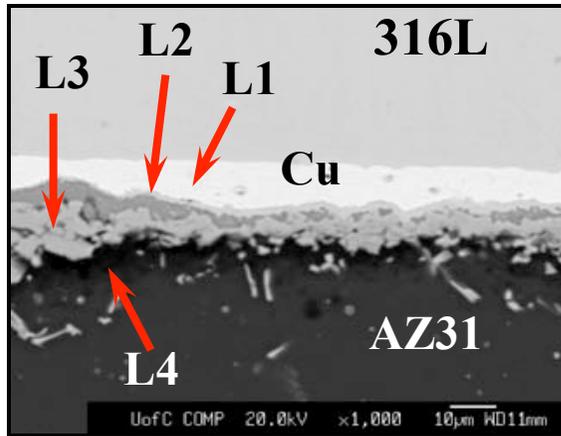
## TLP bonding Process

Steps in the process:

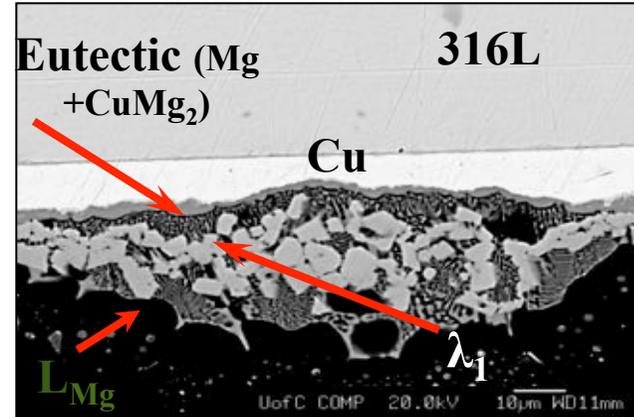
- Solid interlayer
- Interlayer melts
- Isothermal solidification
- Homogenisation



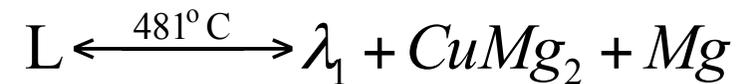
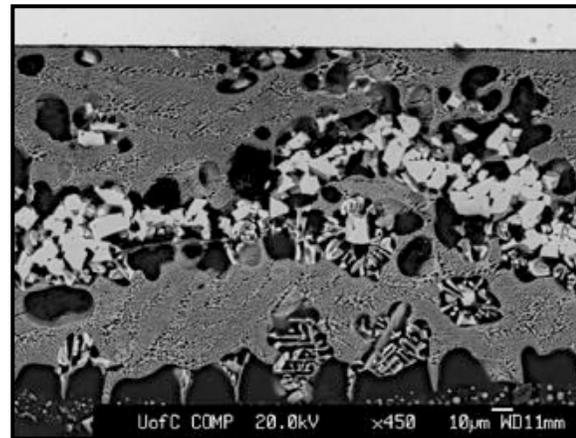
## Bonding Mechanism (Cu interlayer)



**Solid State Diffusion**  
**530°C for 3 min**

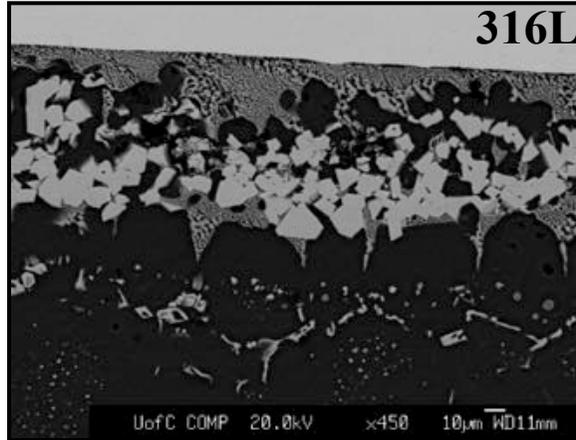


**Eutectic Formation**  
**530°C for 5 min**

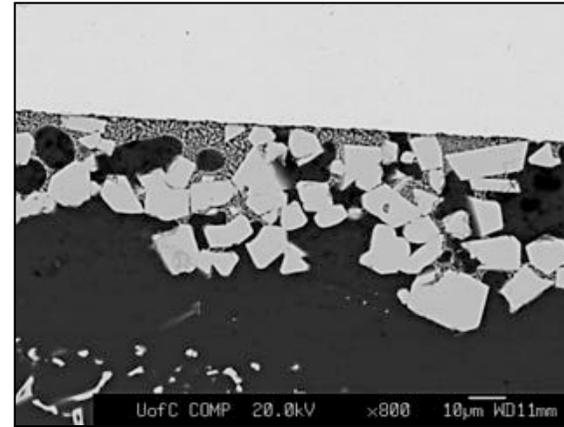


**Dissolution and widening**  
**530°C for 10 min**

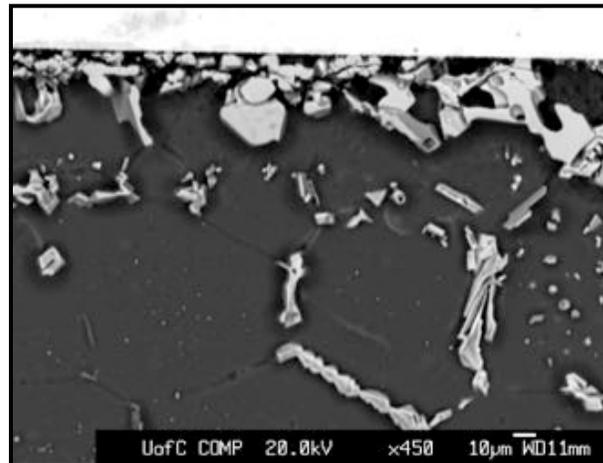
## Isothermal solidification at 530°C (Cu interlayer)



15 min

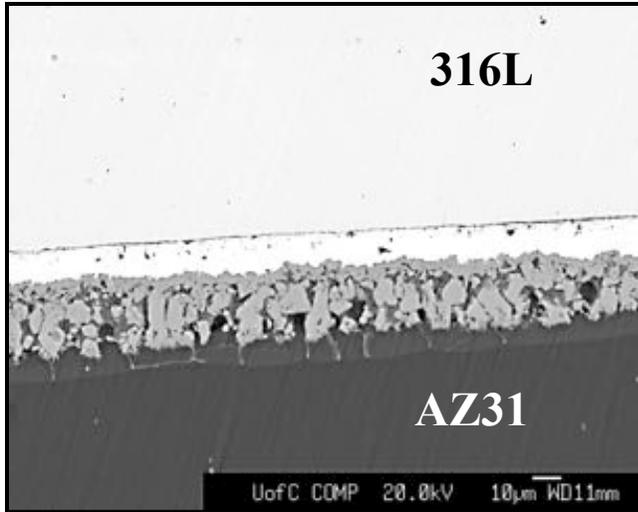


30 min

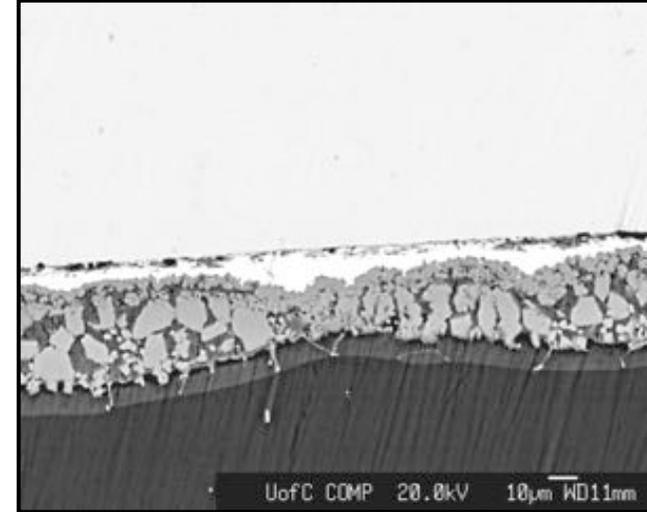


Eutectic dissolution/grain boundary segregation for 60 min

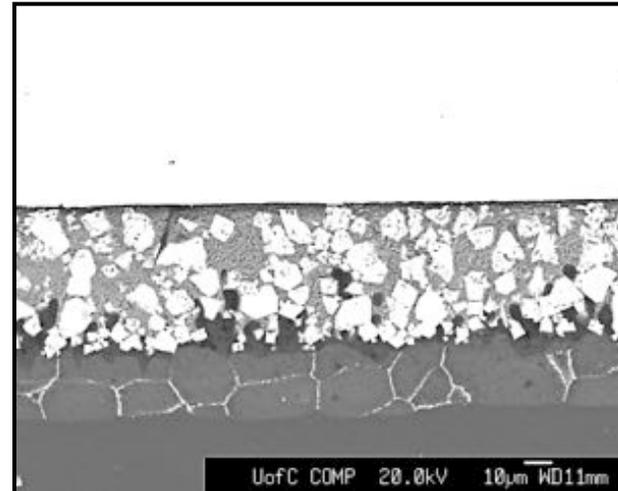
## Bonding Mechanism (Ni interlayer)



510°C for 3 min

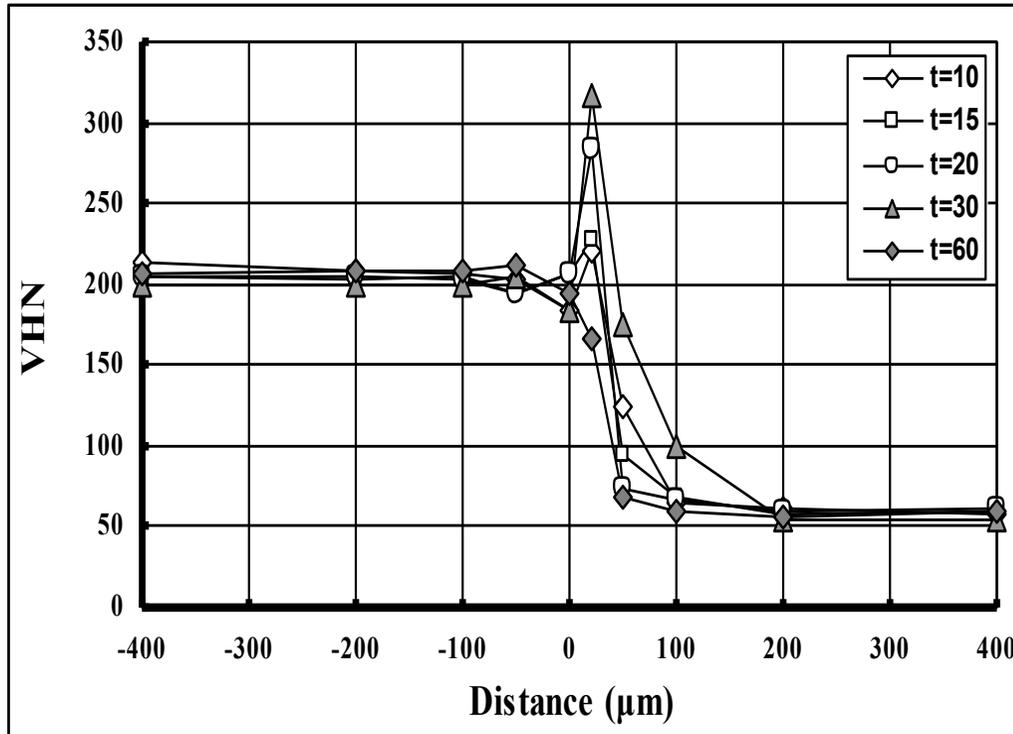


510°C for 5 min



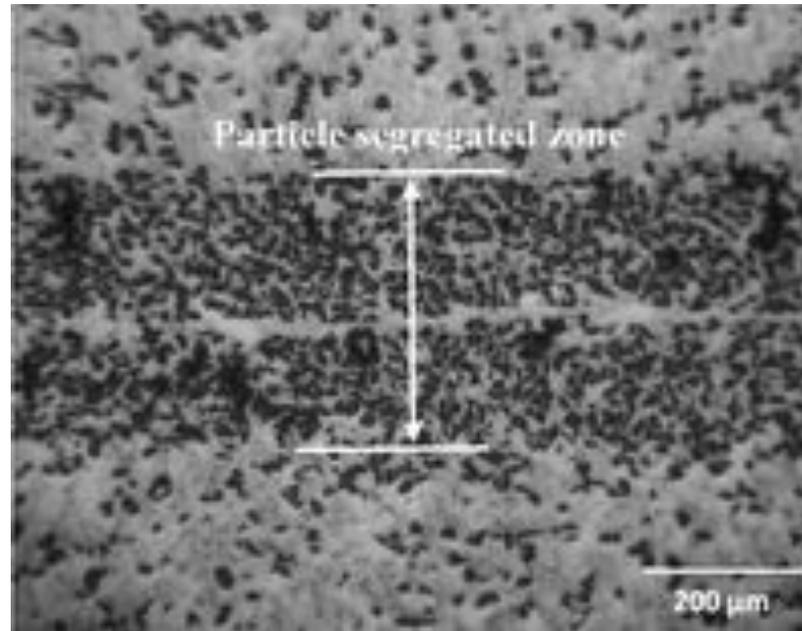
510°C for 10 min

# Effect of bonding time on hardness across joint



AZ31/Cu/316L joint at 530°C

## Al 6061-15% $Al_2O_3$



Microstructure of bond made at 600°C for 10 mins using 15 μm Ni coating.

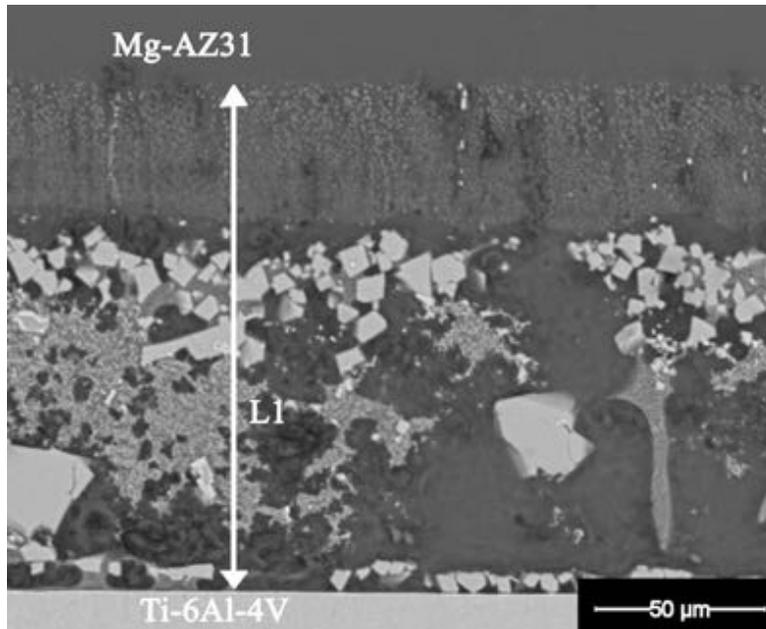
## Problems with TLP bonding

- Dissolution of parent metal;
- Dissolution results in rearrangement of strengthening particles at the joint;
- Bonding time controls isothermal solidification but results in intermetallic compound formation;
- Homogenization time causes grain growth at the joint.

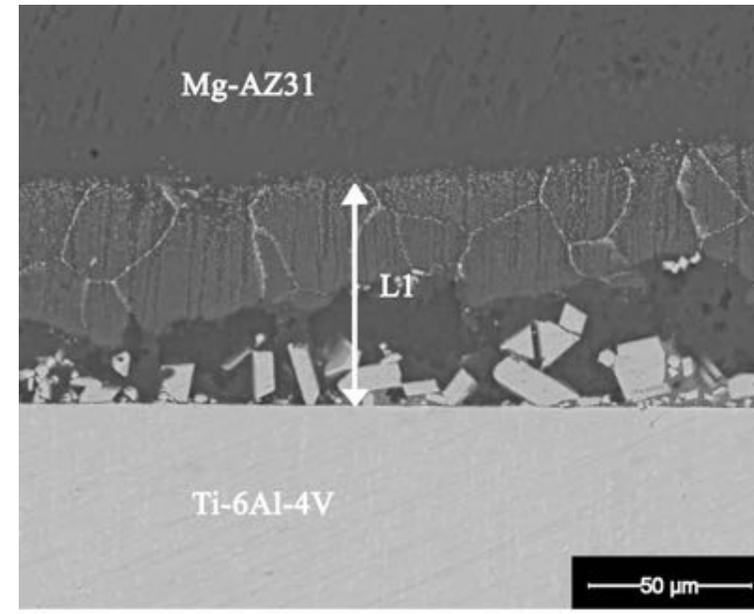
# Potential solutions

- Reduce interlayer thickness;
- Reduce bonding time;
- Select appropriate interlayer composition;
- Use a nanostructured interlayer.

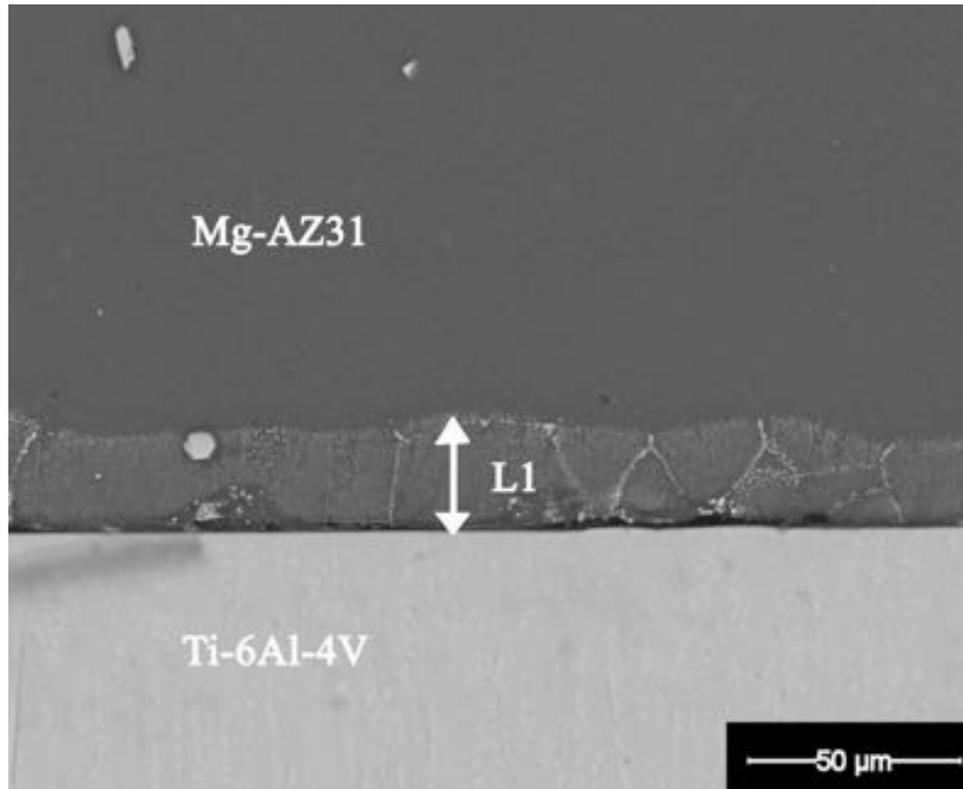
# TLP bonds between Ti-alloy and Mg-alloy using Ni coatings [540°C, 20 mins]



20 μm coating

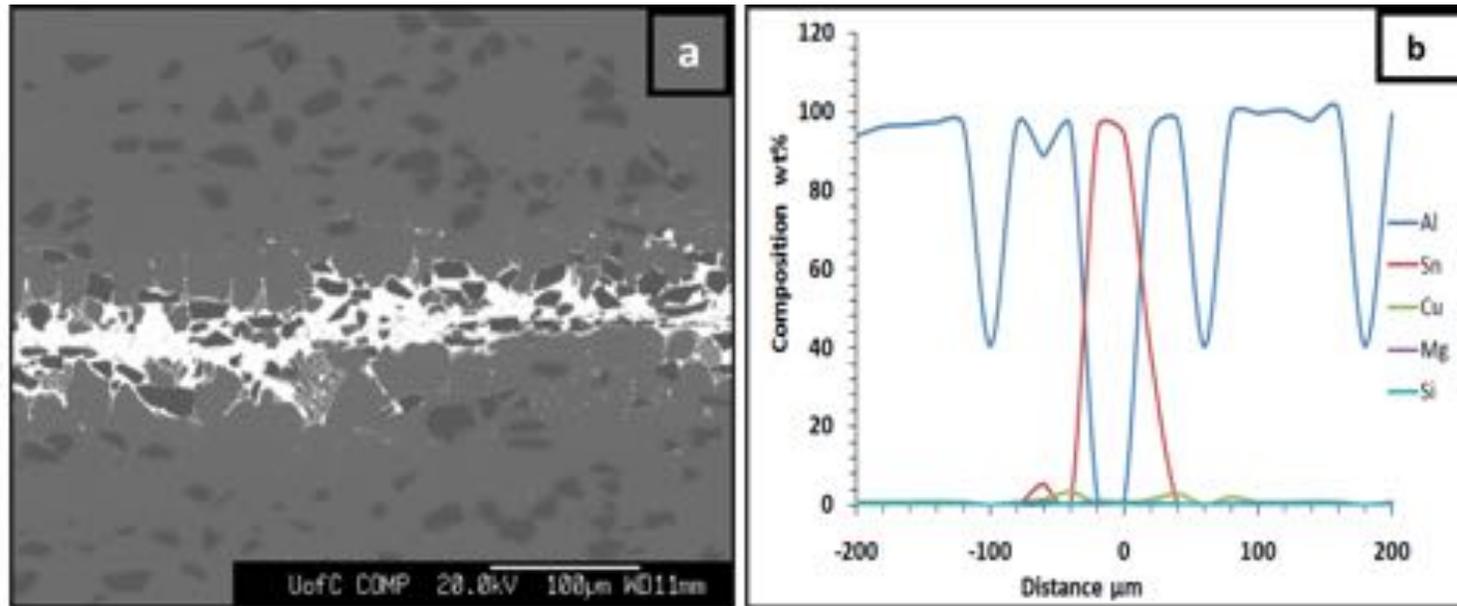


10 μm coating



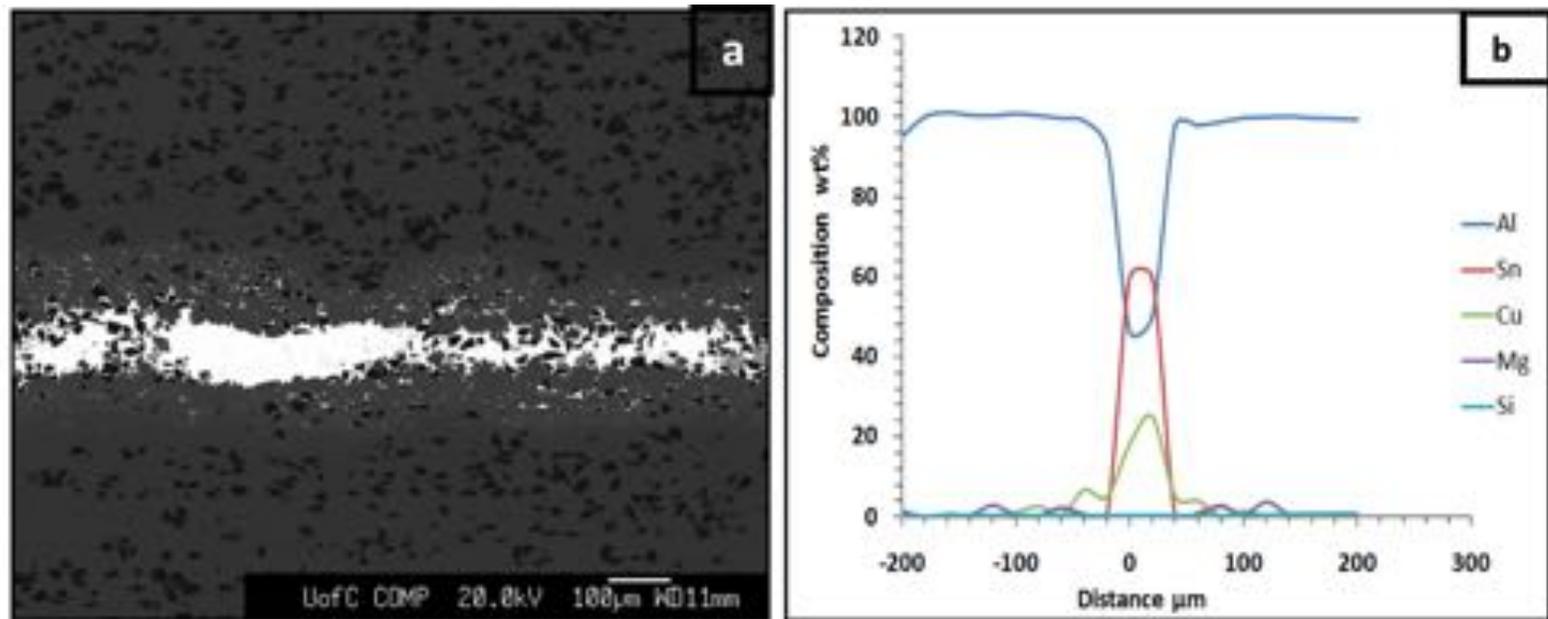
2 μm coating

# Preventing parent metal melt-back



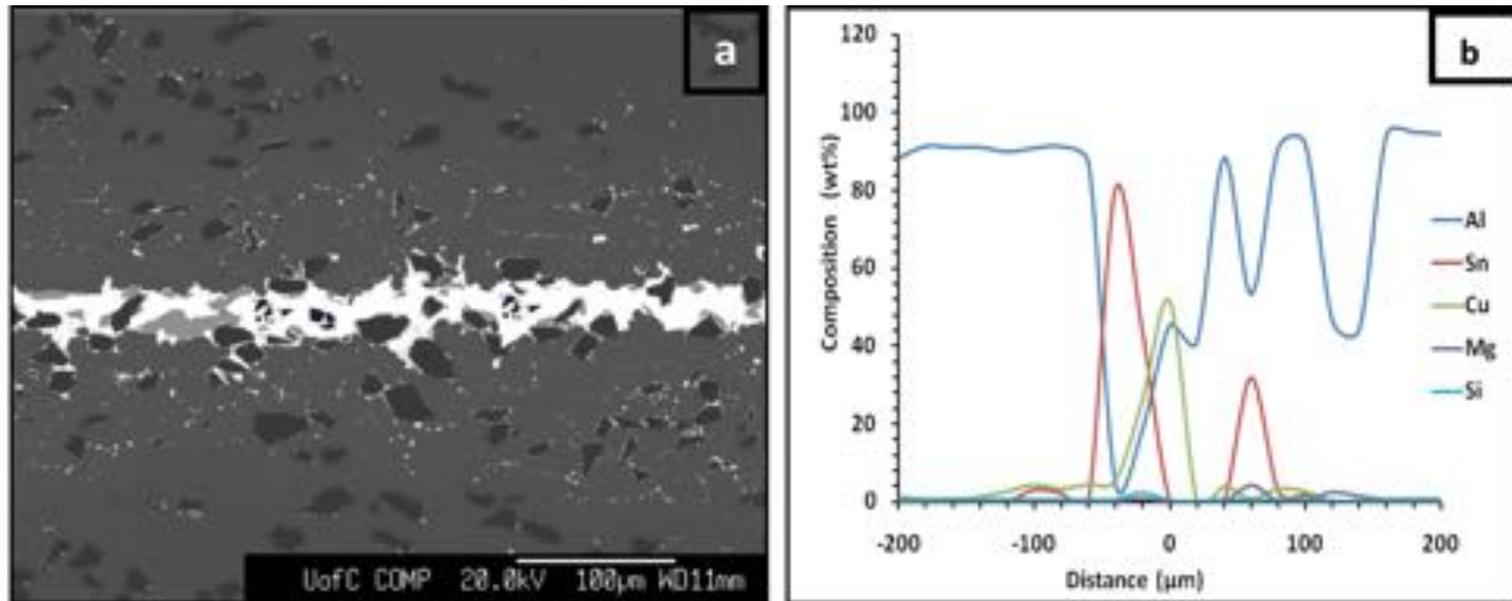
Bond made at 500°C for 2 mins using 5 µm Cu coating on Al-6061 surface and a 50µm Sn interlayer

# Al 6061-15% Al<sub>2</sub>O<sub>3</sub>



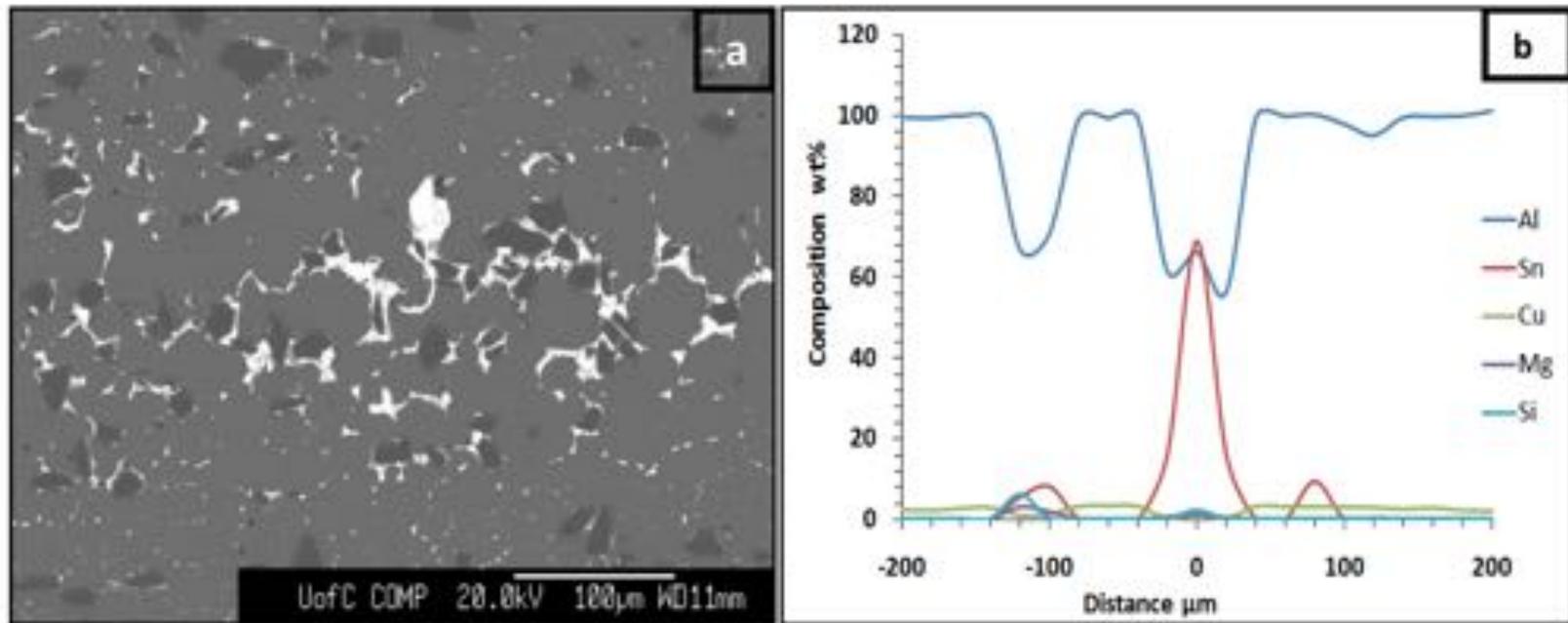
Bond made at 500°C for 30 mins

## Al 6061-15% $\text{Al}_2\text{O}_3$



Bond made at 500°C for 60 mins

## Al 6061-15% Al<sub>2</sub>O<sub>3</sub>



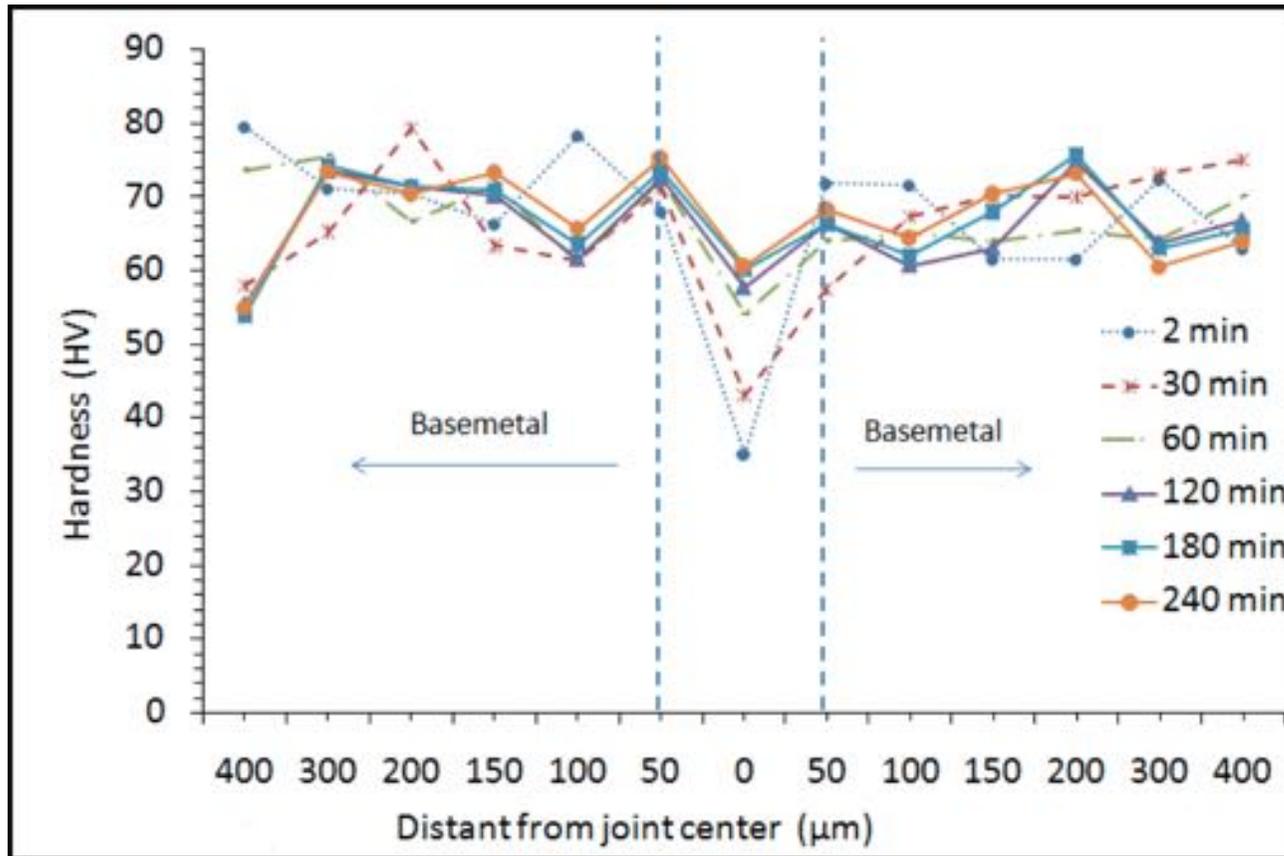
Bond made at 500°C for 180 mins

## Diffusivity values at 500°C for the Al-Cu-Sn system

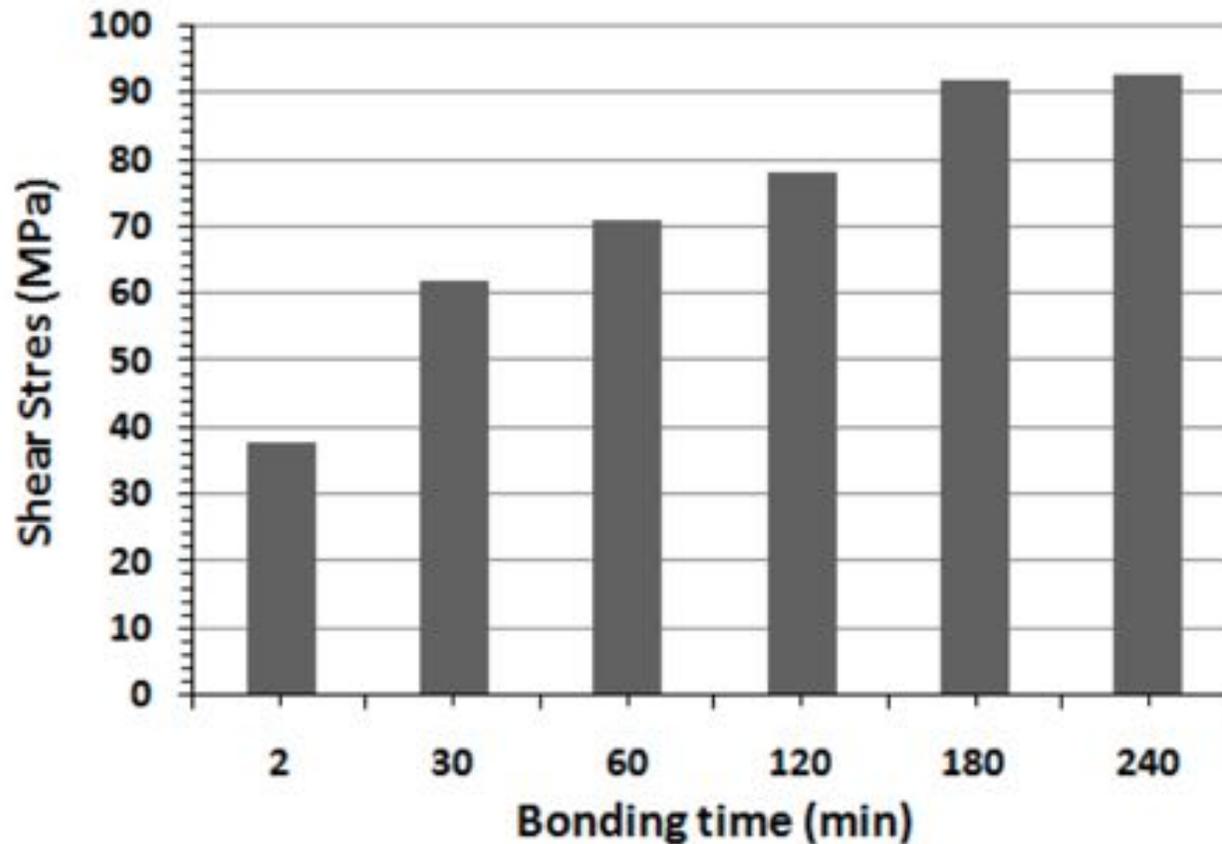
Diffusion type	Diffusivity (D) at 500 °C m <sup>2</sup> /s
Sn in Al	$8.22 \times 10^{-16}$
Sn in Cu	$1.29 \times 10^{-13}$
Cu in Al	$2.58 \times 10^{-9}$
Al in Cu	$2.81 \times 10^{-14}$
Cu in Sn	$1.58 \times 10^{-8}$
Al in Sn	$8.29 \times 10^{-5}$
Mg in Al	$1.54 \times 10^{-9}$



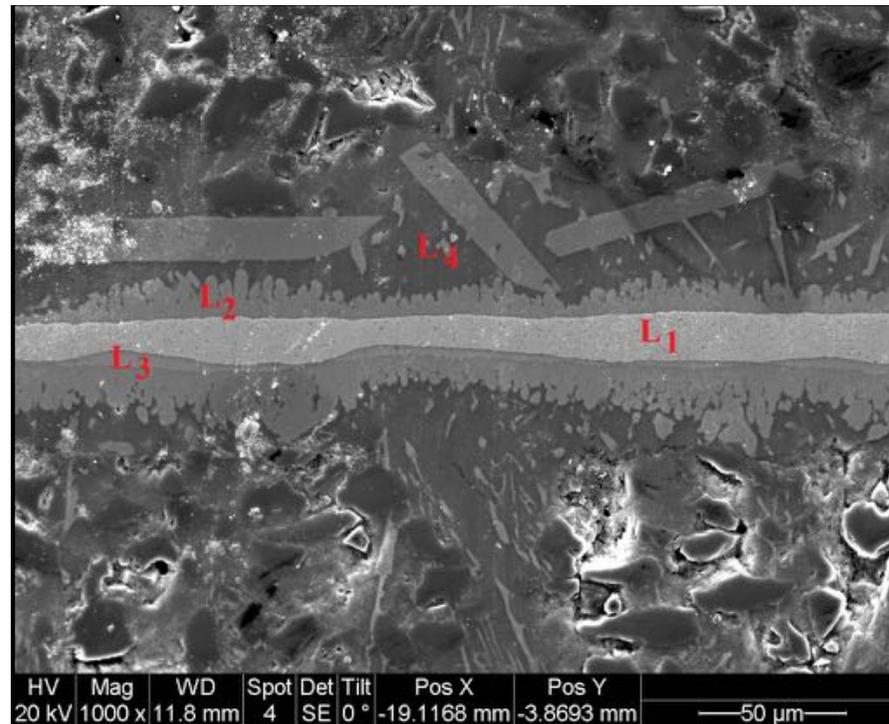
# Changes in hardness across joint made with the Cu-Sn system



# Al-6061 bonds made using Cu-Sn system



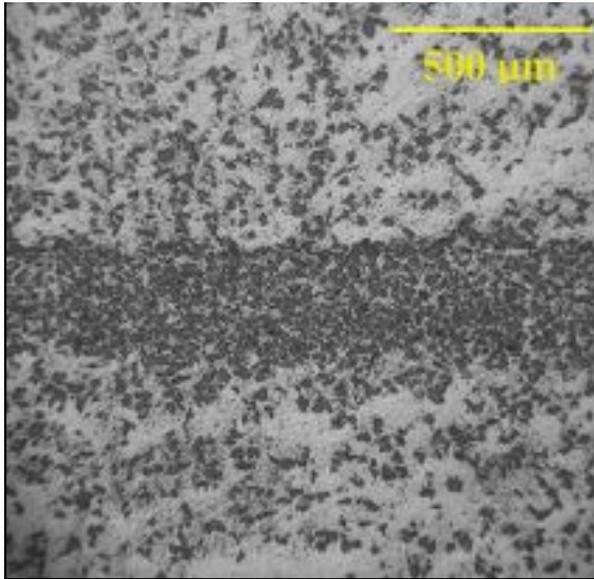
# TLP bond in 6061-15% $\text{Al}_2\text{O}_3$ at 600°C using different Ni coating thickness



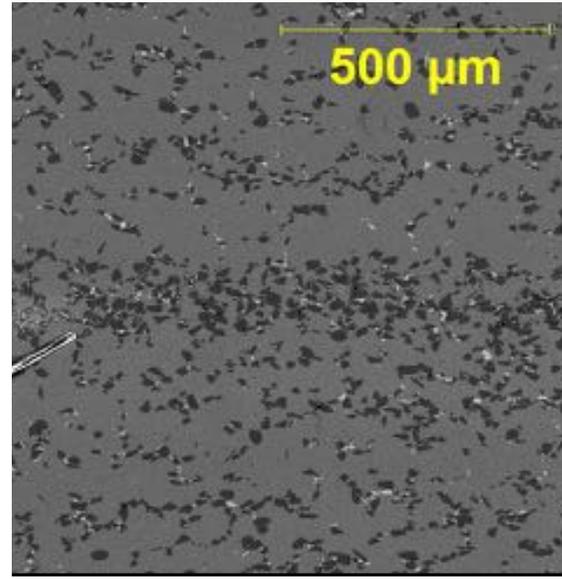
SEM micrograph showing bond made using 15  $\mu\text{m}$  Ni coating for 1 min



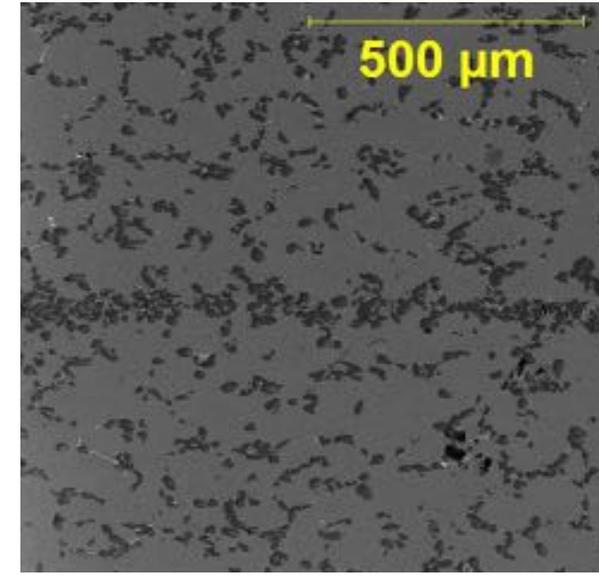
# Effect of Ni-coating thickness on Al-6061-15% Al<sub>2</sub>O<sub>3</sub> at 600°C



15 μm

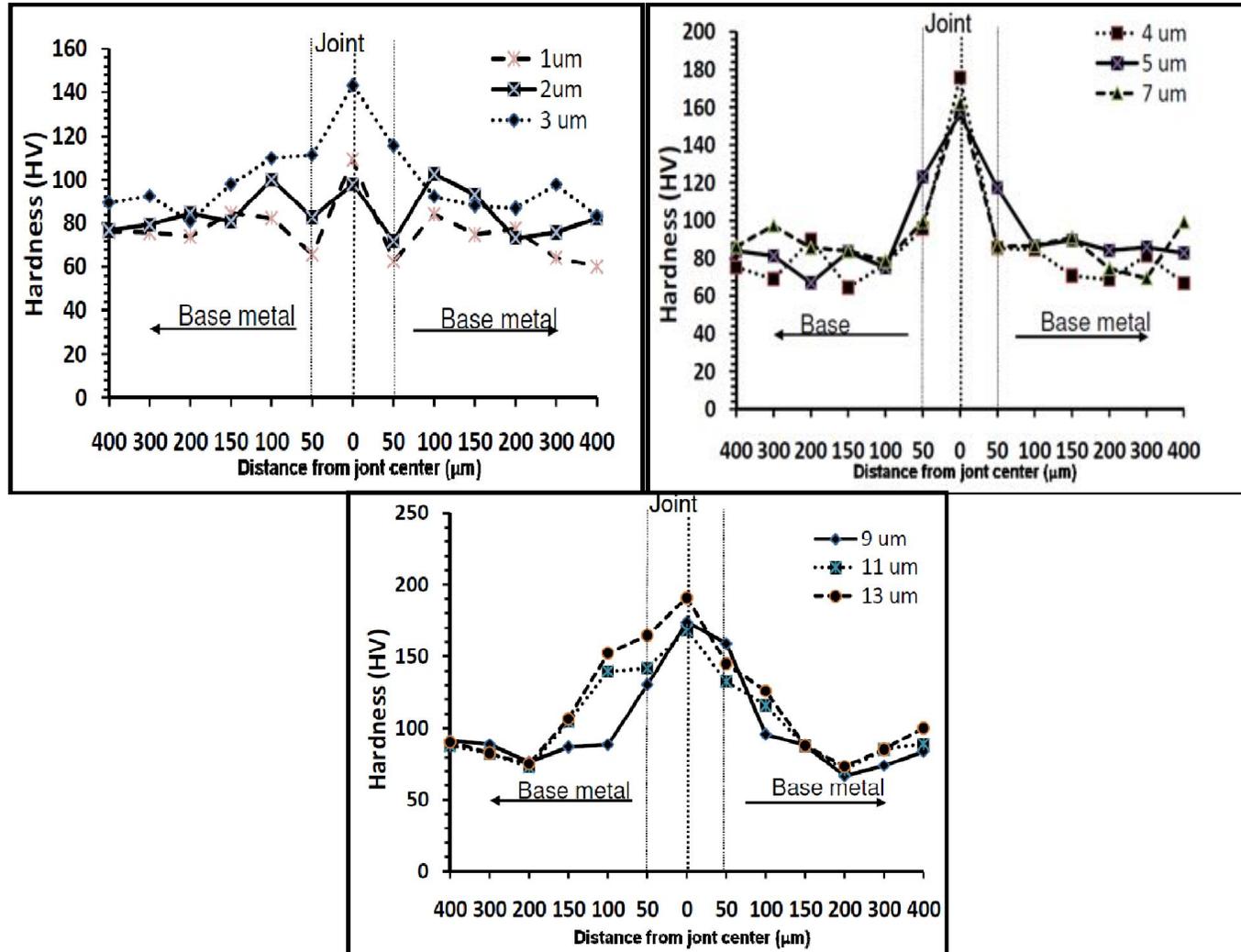


5 μm

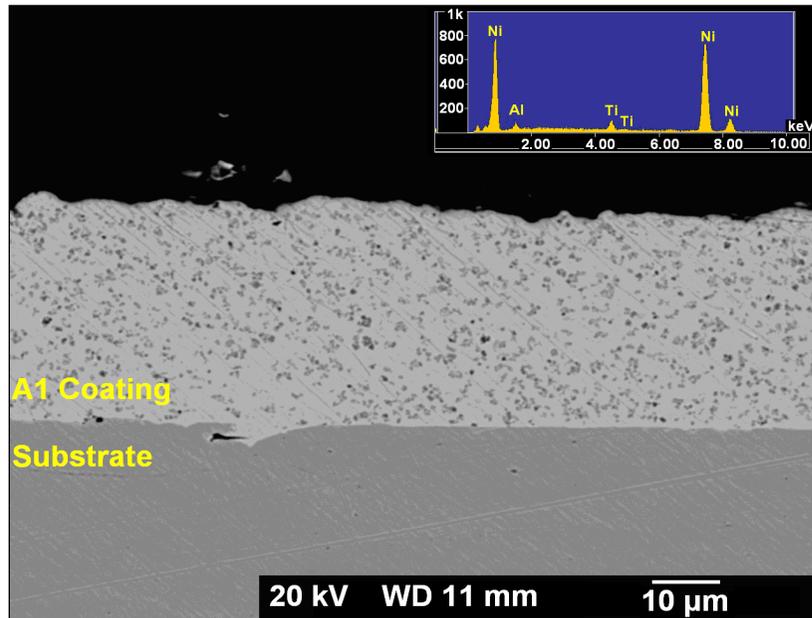


2 μm

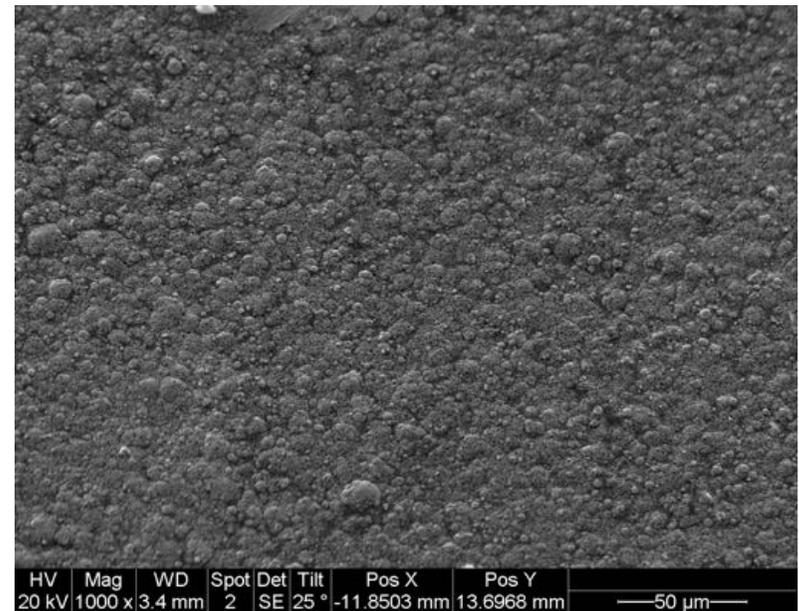
## Changes in hardness at the joint as a function of coating thickness



# Ni-coating containing nano-particles



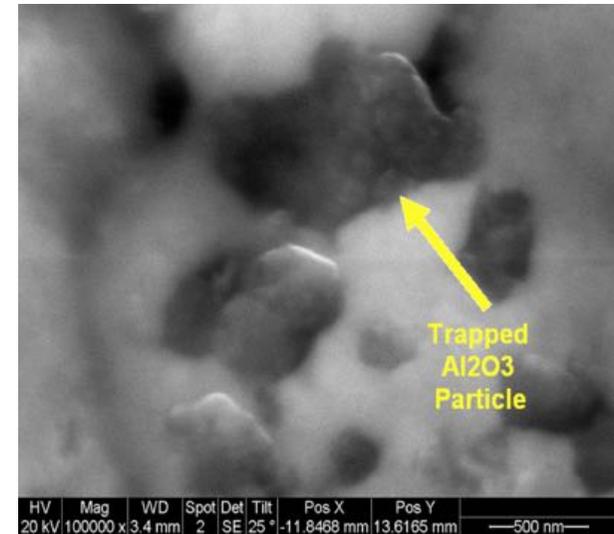
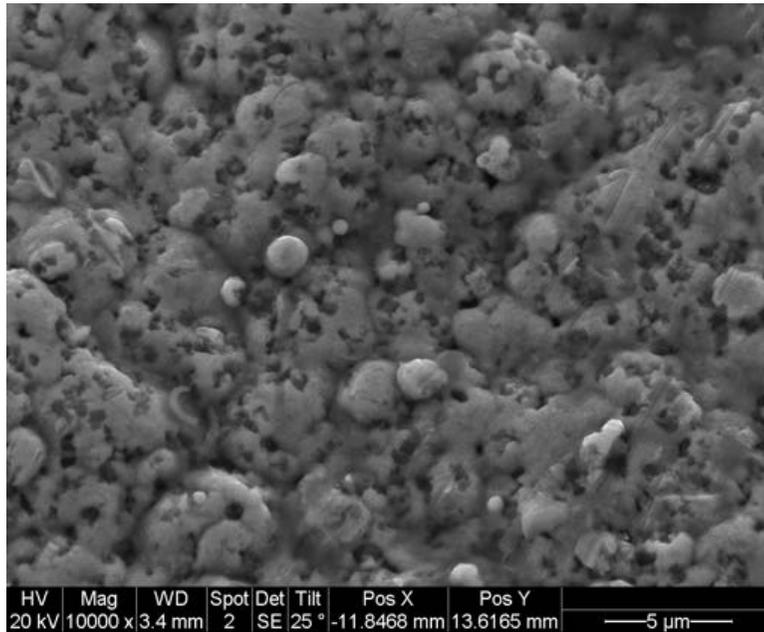
(a)



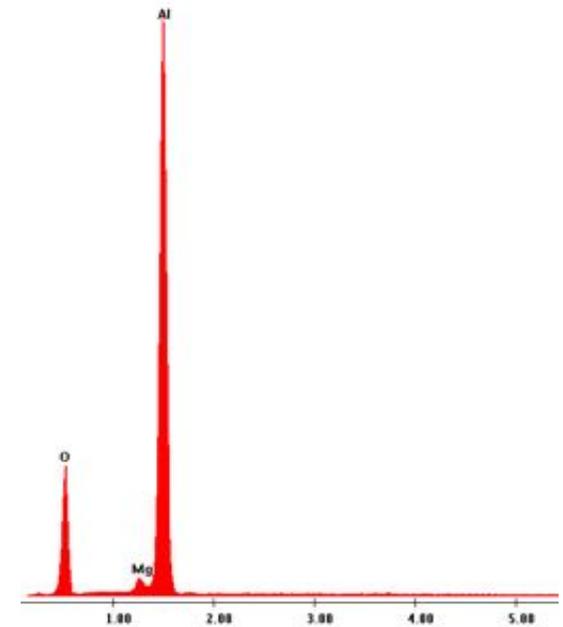
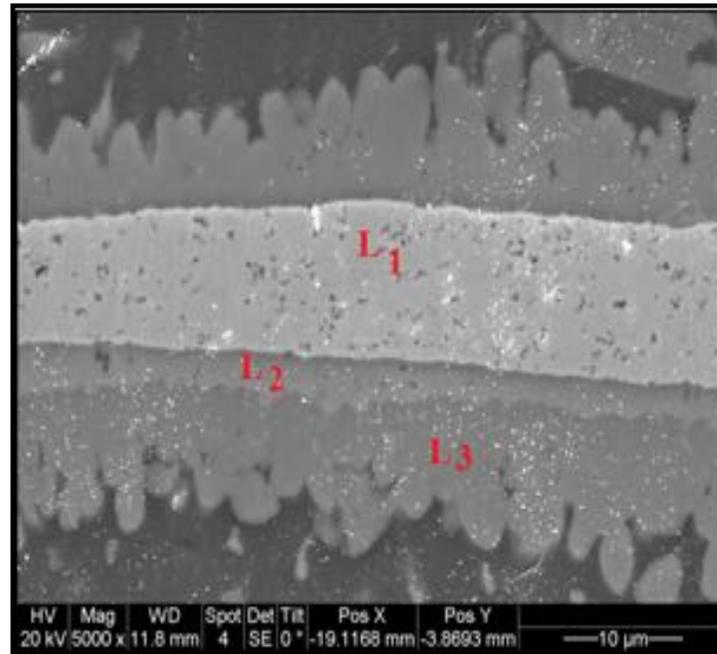
(b)

SEM micrographs showing:  
(a) cross-section through Ni coating; (b) surface morphology

# Dispersion of $\text{Al}_2\text{O}_3$ nano-particles in the Ni coating



# TLP bonds in 6061-15% $\text{Al}_2\text{O}_3$ at 600°C using nano-particles



SEM micrograph of joint bonded using a 15  $\mu\text{m}$  Ni- $\text{Al}_2\text{O}_3$  coating for 1 min

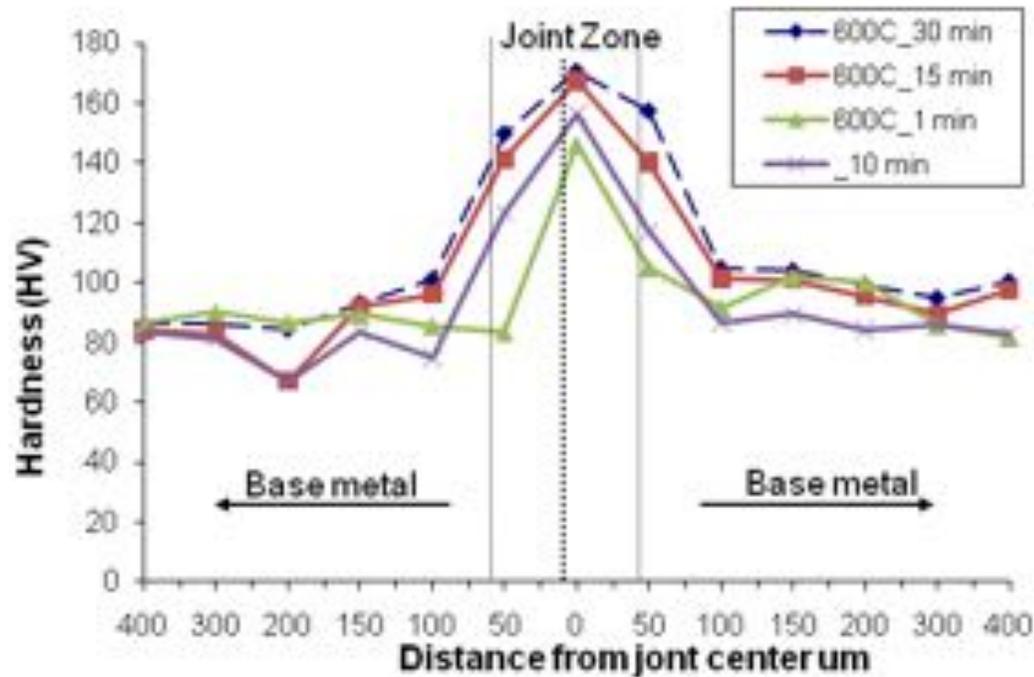


## EDS quantitative analysis of reaction layers

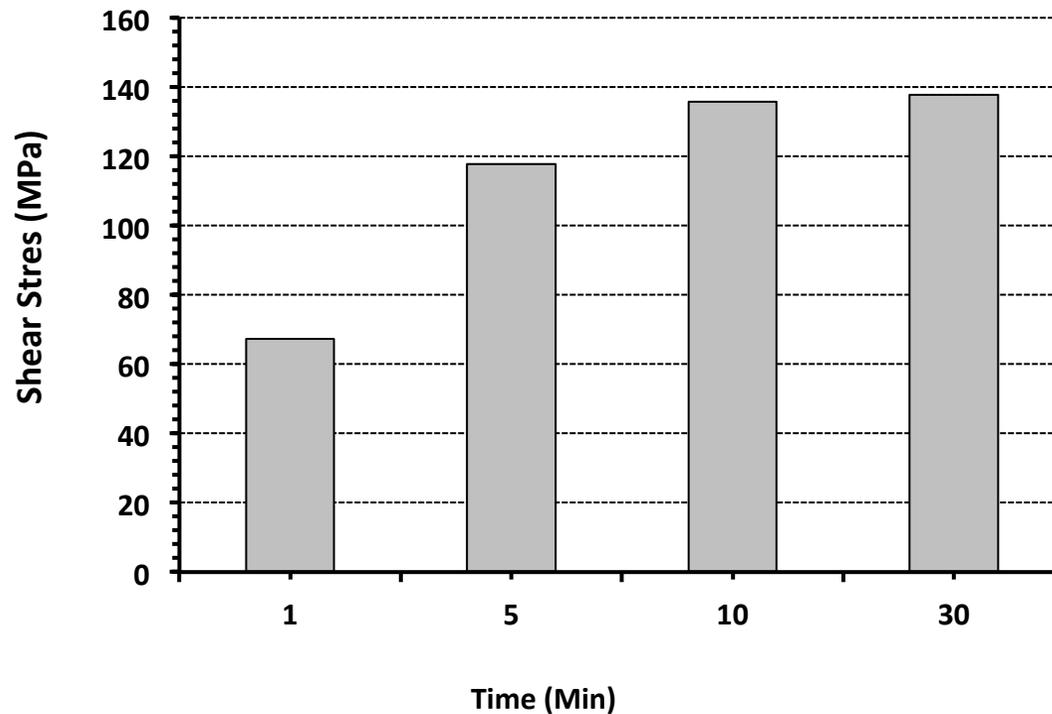
Layers	Al	Ni	Si	Mg	Compound
L <sub>1</sub>	12.5	87.5	0	0	Ni + Al <sub>2</sub> O <sub>3</sub>
L <sub>2</sub>	46.71	50.67	0.27	0	NiAl
L <sub>3</sub>	72.84	24.31	0	0.55	NiAl <sub>3</sub>
L <sub>4</sub>	72.84	24.31	0	0.55	NiAl <sub>3</sub>



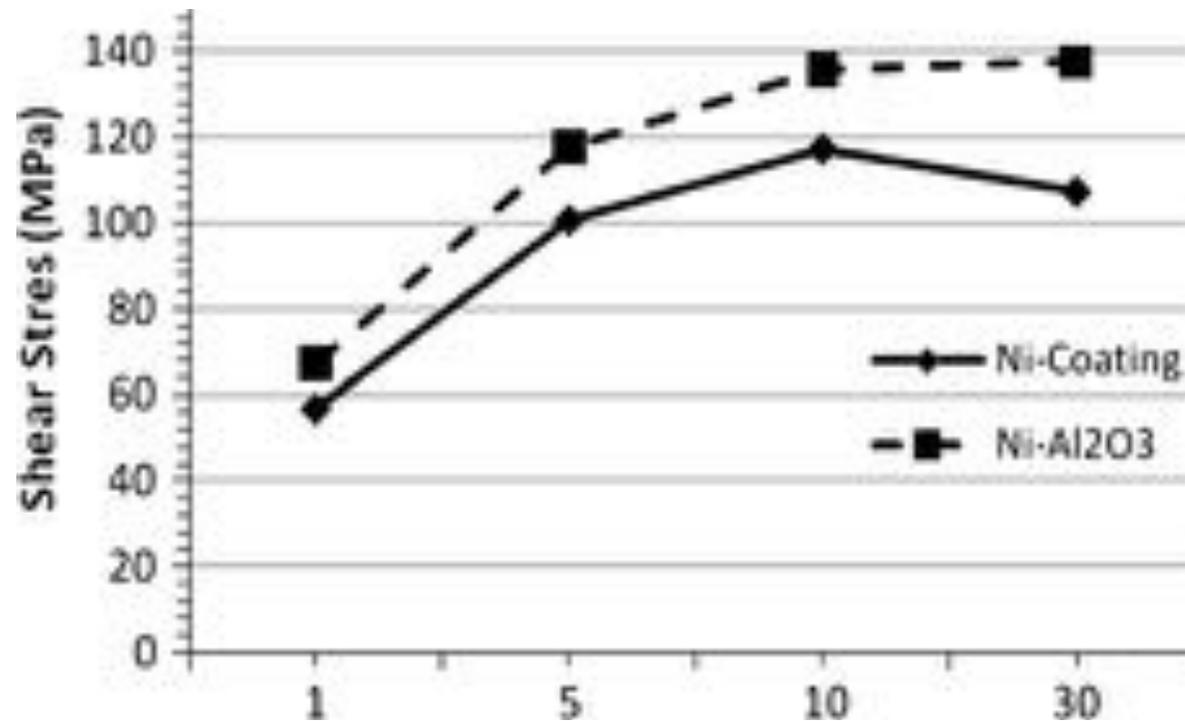
# TLP bonds in 6061-15% $\text{Al}_2\text{O}_3$ at 600°C



# TLP bond strengths using 5 $\mu$ m thick Ni- Al<sub>2</sub>O<sub>3</sub> coating made at 600°C

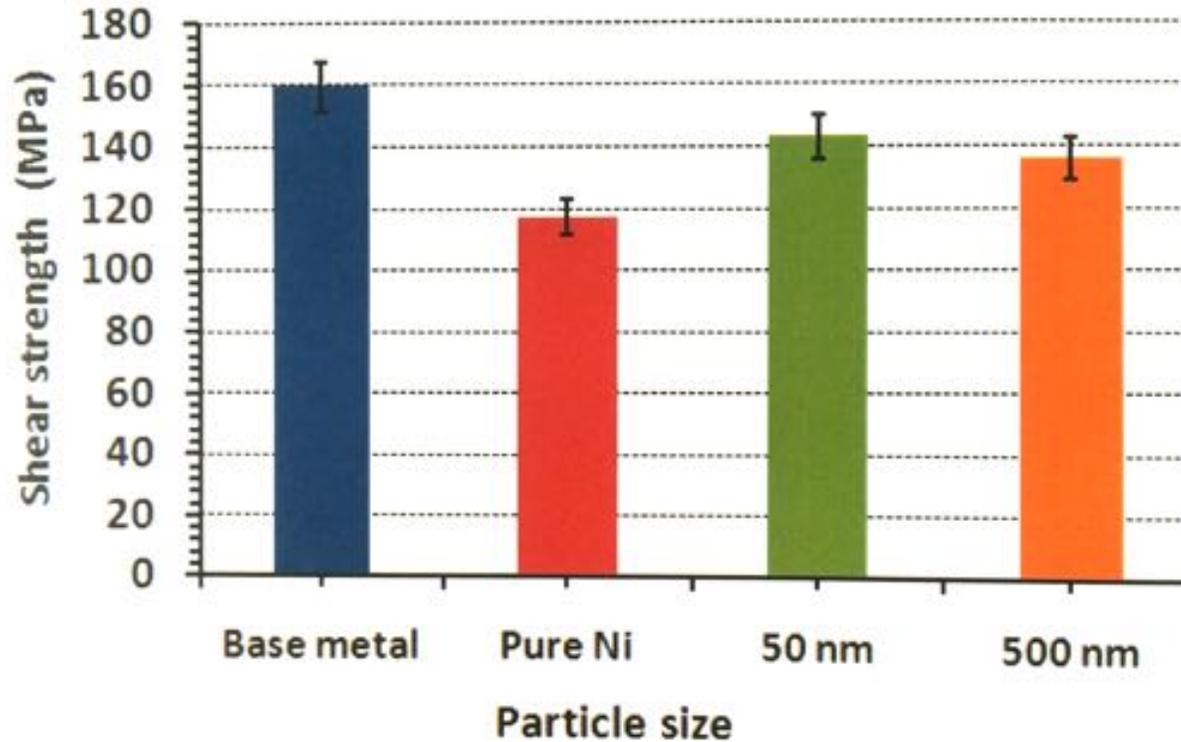


## Effect of nano-particles on joint strength

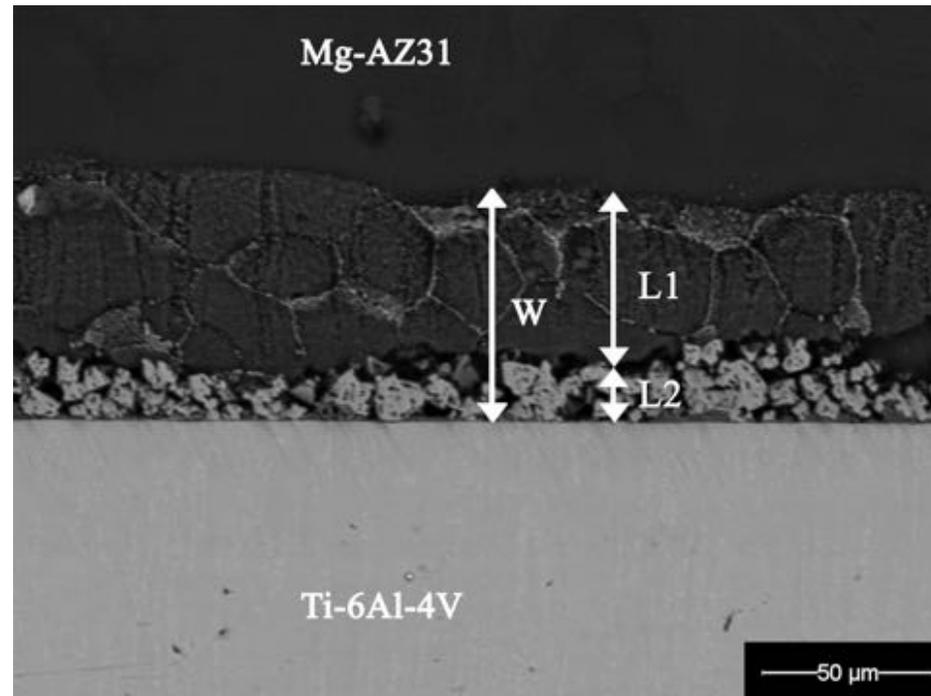




# Effect of nano-particle size

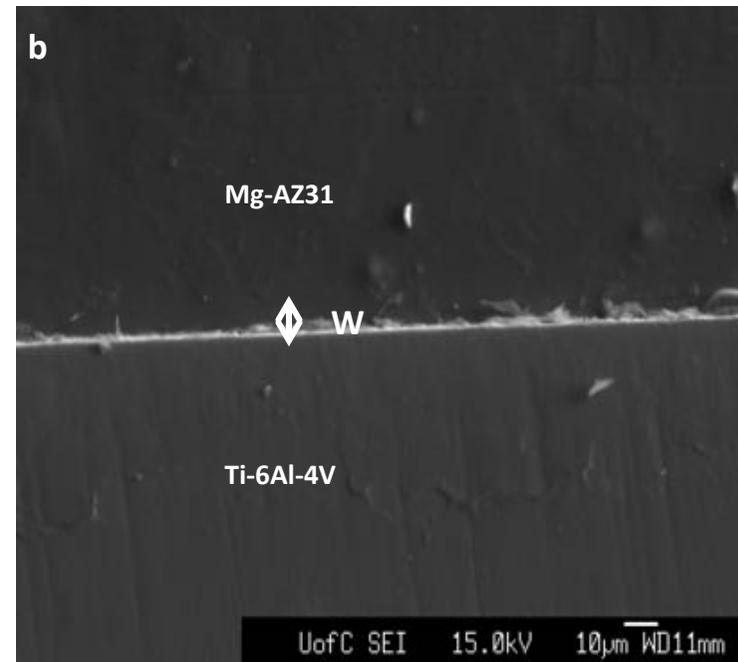
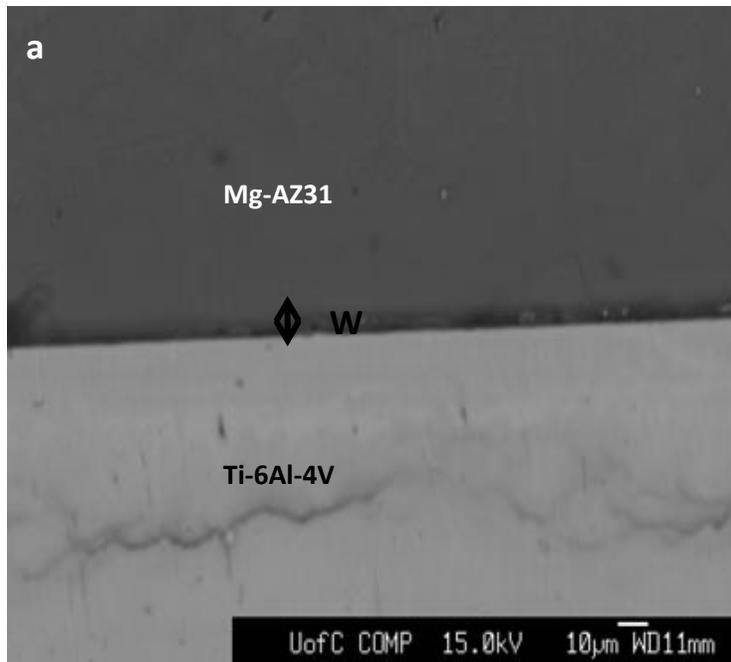


# TLP bonds made with Ni coating containing Ni nanoparticles



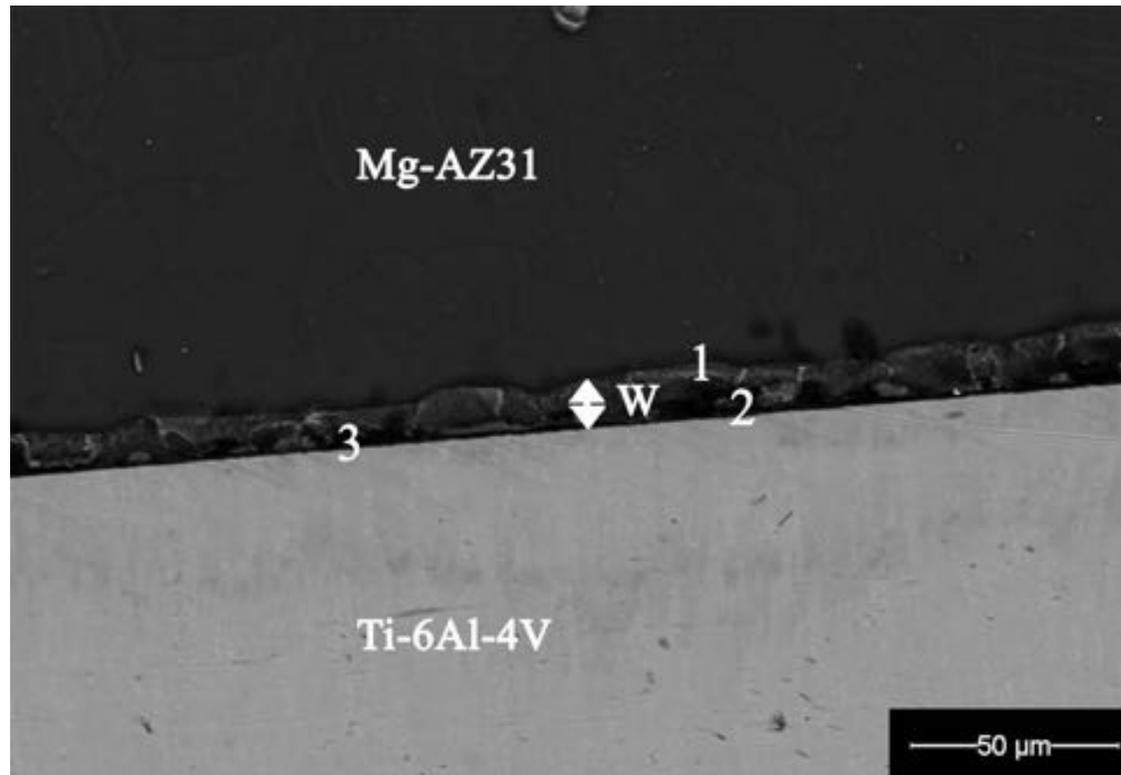
10 μm coating thickness [520°C, 20 min]

# TLP bonds made with Ni coating containing Cu nanoparticles



10 µm coating thickness [520°C, 20 min]

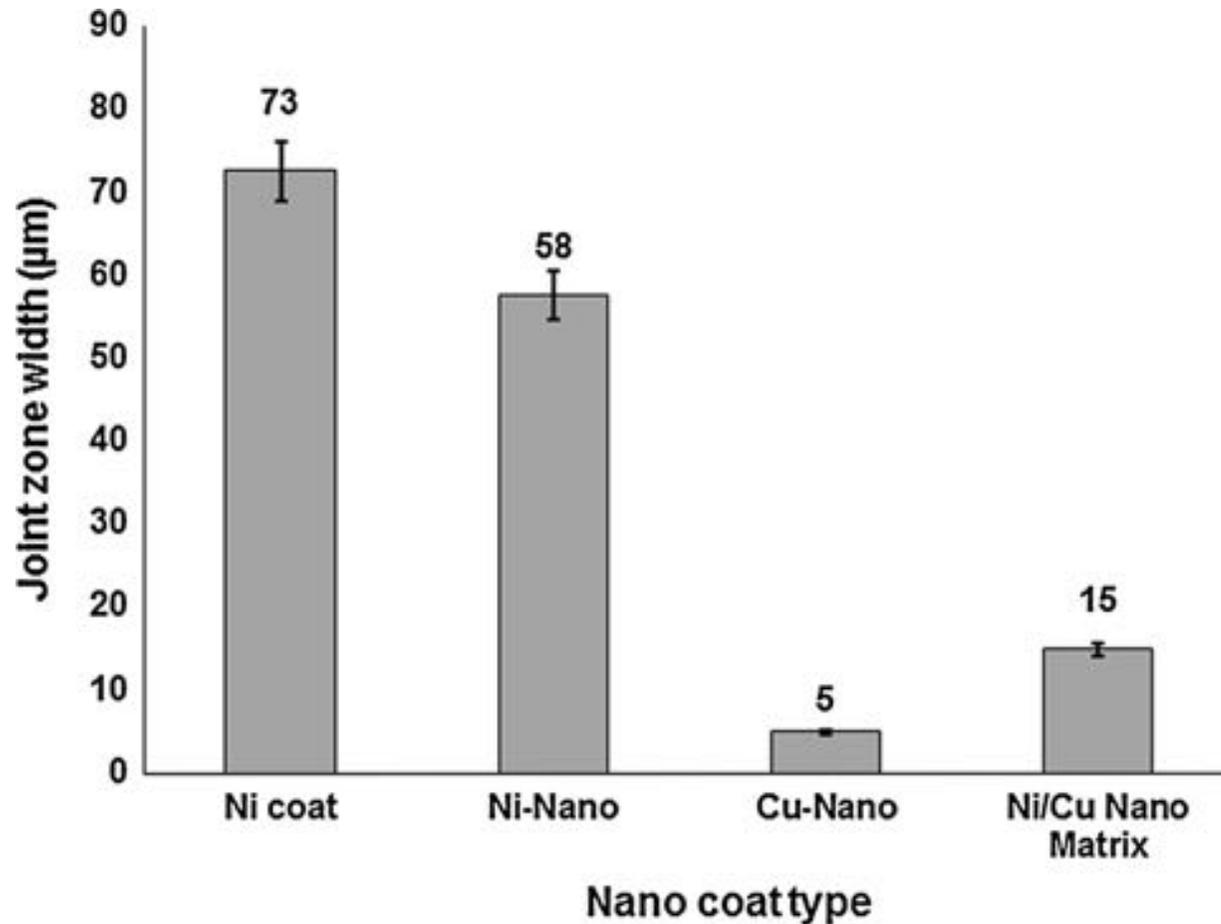
# TLP bonds made with Ni coating containing Cu-Ni nanoparticles



10 μm coating thickness [520°C, 20 min]

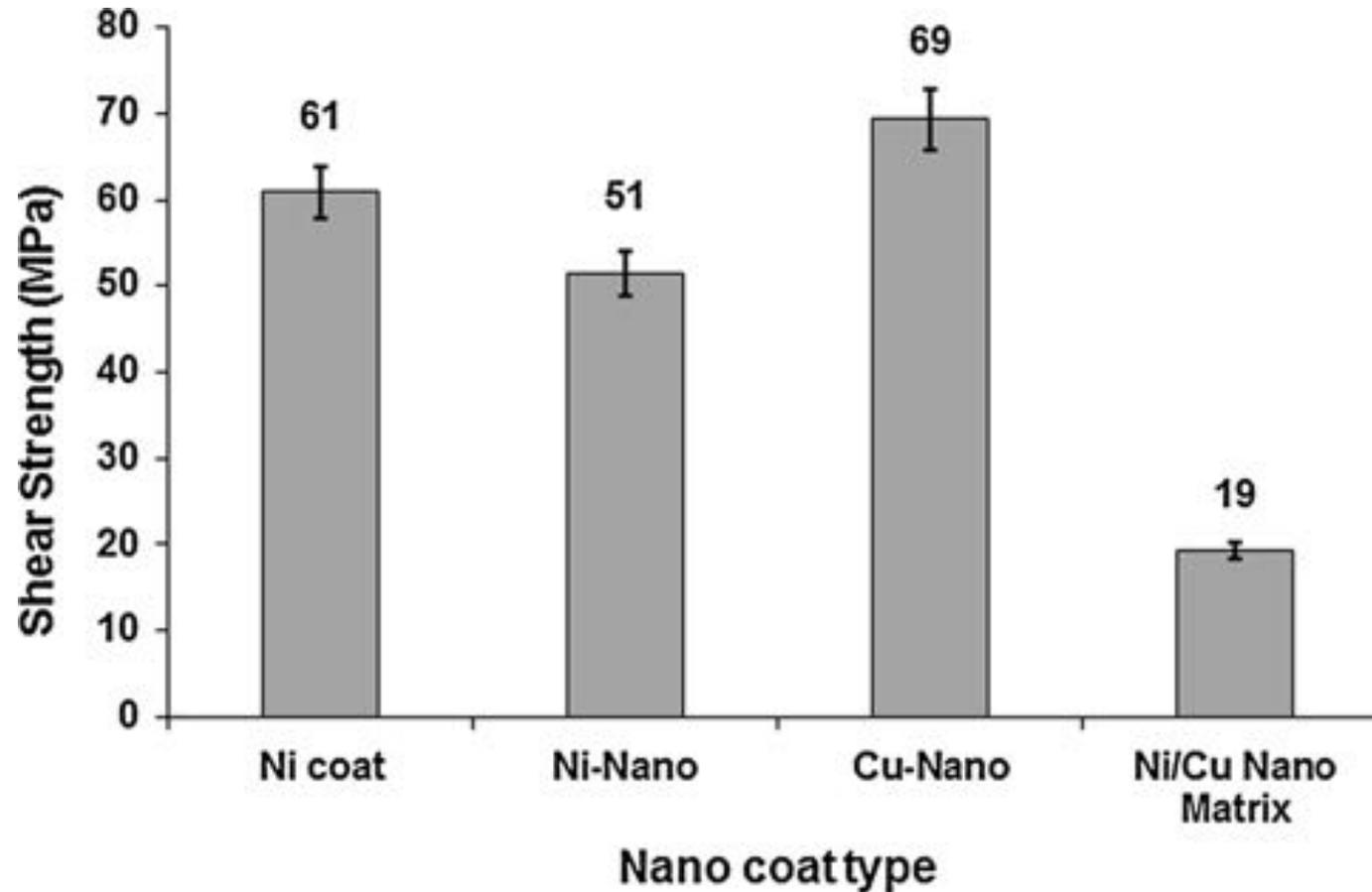


# Effect of nanoparticles on eutectic width

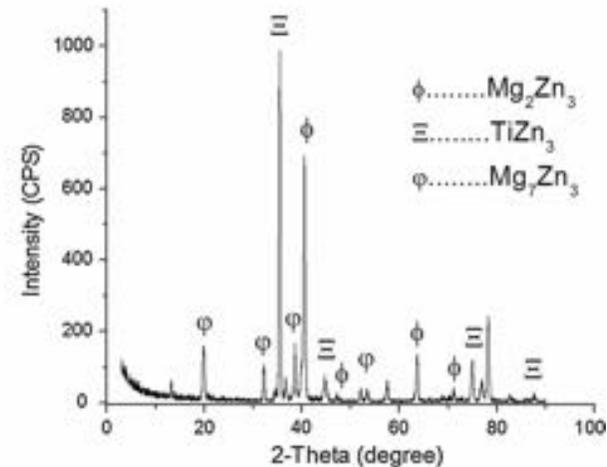
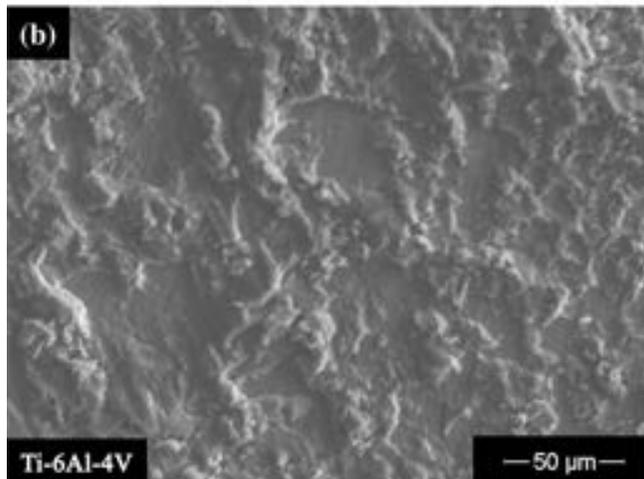
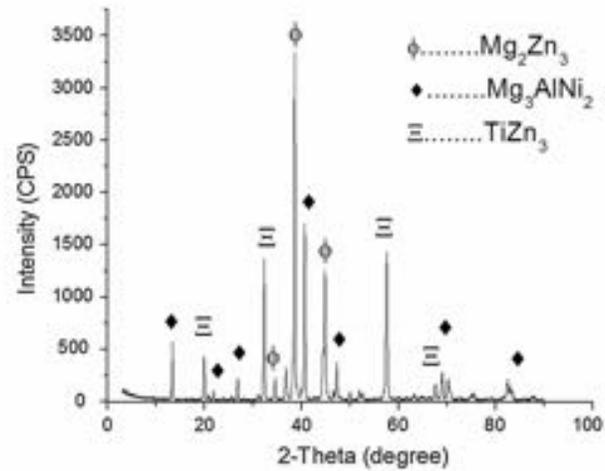
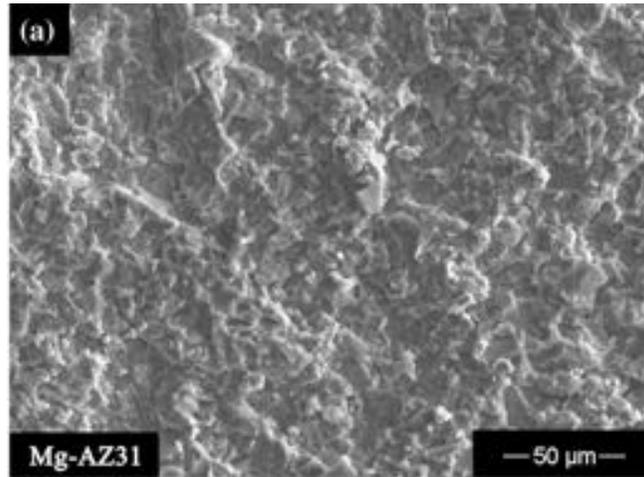




# Joint shear strengths



# Ti-6Al-4V/Ni nano/Mg-AZ31



## Summary

- ❖ Dissolution and melt-back is reduced using thinner interlayers;
- ❖ Nano-particles can be used to reduce the eutectic liquid thickness and increase solidification rate;
- ❖ Nano-particles present in the interlayer can provide greater joint strengths than using pure metal interlayers;
- ❖ The size of the nano-particles used as a dispersion affect the extent of strengthening.

# Acknowledgements

## Research Team at University of Calgary

